

SÃO PAULO UNIVERSITY
SCHOOL OF ENGINEERING OF SÃO CARLOS
DEPARTAMENT OF STRUCTURAL ENGINEER
LABORATORY OF WOOD AND TIMBER STRUCTURES



LaMEM

South America Timber Structures Code



Prof. Carlito Calil Junior



LaMEM

Introduction

- South America don't have a unified code for the design of timber structures
- European Standards
- hardwoods in South America
- Allowable Stress Design of 1982
- Limit States Design concept
- NBR7190 in 1997



LaMEM

LaMEM - SET - EESC - USP

Loads

- Upper 95 characteristic value
- impact situation the code reduces the live load factor of 0.75 in the loads combination.
- maximum and minimum values used to produce the more critical combinations



LaMEM

Material Properties

- The properties to consider in design of timber structures are: density, strength, stiffness and moisture content
- The specified properties of strength and stiffness corresponds to the class of moisture content of 12%, that is 25 degrees Celsius and 65% of relative humidity



LaMEM

Characterization of Wood Properties

- complete and the minimum strength characterization of wood properties ,
- simplified characterization of strength ,
- compression parallel to grain tests ,
- normal stress allows a variation coefficient of 18%
- to tangential stress allows a variation coefficient of 28%



LaMEM

LaMEM - SET - EESC - USP

Strength Classes

- Eight classes are defined: three for softwoods, prefixed C, and five for hardwoods, prefixed D ,
- The softwood strength classes are C20(weakest), C25 and C30 ,
- The hardwood strength classes are D20, D30, D40, D50 and D60 ,
- characteristic compression parallel to grain stress for each strength class



LaMEM

Hardwood Graded to NBR7190/2008(draft,

Table 1 Strength class for hardwoods.

Strength Classes	$f_{c0,k}$ (MPa)	$f_{v0,k}$ (MPa)	$E_{c0,m}$ (MPa)	$\rho_{bas,m}$ (kg/m ³)	$\rho_{ap,m,12\%}$ (kg/m ³)
C20	20	4	9500	500	650
C30	30	5	14500	650	800
C40	40	6	19500	750	950
C50	50	7	22000	770	970
C60	60	8	24500	800	1000



Softwood graded to NBR7190/2007

Table 2 Strength class for softwoods.

Strength Classes	$f_{c0,k}$ (MPa)	$f_{v0,k}$ (MPa)	$E_{c0,m}$ (MPa)	$\rho_{bas,m}$ (kg/m³)	$\rho_{ap,m,12\%}$ (kg/m³)
C 20	20	4	3 500	400	500
C 25	25	5	8 500	450	550
C 30	30	6	14.500	500	600



LaMEM

Representative Strength and Stiffness Values

$$X_d = k_{\text{mod}} \frac{X_k}{\gamma_w}$$

$$k_{\text{mod}} = k_{\text{mod},1} \cdot k_{\text{mod},2} \cdot k_{\text{mod},3}$$



LaMEM

LaMEM - SET - EESC - USP

load classes and types of materials

Table 3 – Values of $k_{mod,1}$

Load Classes	Sawn wood, Glulam, Plywood	Recomposed wood
Dead load	0,60	0,30
Long duration load	0,70	0,45
Médium duration load	0,80	0,65
Short duration load	0,90	0,90
Instantaneous	1,10	1,10

classes of moisture content and types of materials

Table 4 – Values of $k_{mod,2}$

Classes of moisture content	Sawn wood, Glulam, Plywood	Recomposed wood
(1) e (2)	1,0	1,0
(3) e (4)	0,8	0,9

(1) corresponds a 12% moisture content wood and relativity humidity $< 65\%$

(2) corresponds a 15% moisture content wood and $65\% < U_{amb} \leq 75\%$ relativity humidity

(3) corresponds a 18% moisture content wood and $75\% < U_{amb} \leq 85\%$ relativity humidity

(4) corresponds a 25% moisture content wood and relativity humidity $> 85\%$



LaMEM



LaMEM

grading of wood

Table 5a. Proposed values of $k_{mod, 3}$ for hardwoods.

Class	$k_{mod,3}$ (visual +proof test)	$k_{mod,3}$ (visual+transversal vibration)	$k_{mod, 3}$ (visual + stress wave)
SE	1,00	0,95	0,90
S1	0,95	0,90	0,85
S2	0,90	0,85	0,80
S3	0,85	0,80	0,75



LaMEM

grading of wood

Table 5b. Proposed values of $k_{mod, 3}$ for softwoods - D.

Class	$k_{mod,3}$ (visual +proof test)	$k_{mod,3}$ (visual+transversal vibration)	$k_{mod, 3}$ (visual + stress wave)
SE-D	1,00	0,90	0,85
S1-D	0,95	0,85	0,80
S2-D	0,90	0,80	0,75
S3-D	0,85	0,75	0,70



LaMEM

grading of wood

Table 5c. Proposed values of $k_{mod, 3}$ for softwoods - ND.

Classe	$k_{mod,3}$ (visual +proof test)	$k_{mod,3}$ (visual+transversal vibration)	$k_{mod, 3}$ (visual + stress wave)
SE-ND	1,00	0,85	0,80
S1-ND	0,95	0,80	0,75
S2-ND	0,90	0,75	0,70
S3-ND	0,85	0,70	0,65

Partial Safety Factors for Ultimate Limit States

-the partial factor for compression parallel and normal to grain is

$$\gamma_{wc} = 1,4$$

-the partial factor for tension parallel to grain is

$$\gamma_{wt} = 1,8$$

-the partial factor for shear is

$$\gamma_{wv} = 1,8$$



LaMEM

LaMEM - SET - EESC - USP



LaMEM

Stiffness

the elasticity modulus parallel to grain must be taken as:

$$E_{co,ef} = k_{mod,1} \cdot k_{mod,2} \cdot k_{mod,3} \cdot E_{co,m}$$

And the transversal modulus as:

$$G_{ef} = E_{c0,ef} / 20$$



LaMEM

LaMEM - SET - EESC - USP

Design Considerations in Stability of Compression Elements

- accidental eccentricity loads and geometrical lumber imperfections
- accidental eccentricity value of $L/300$
- $\lambda > 40$ must be designed for bending and compression

$$e_i = \frac{M_{1d}}{N_d} \quad \text{- design eccentricity}$$

$$e_1 = e_i + e_a \quad e_a = L_o/300 \quad \text{- accidental eccentricity}$$



LaMEM

Mechanical Connections

For mechanical connections of wood members the code presents three types of elements:

- steel dowels or bolts
- wood dowels
- steel rings and metal plate connectors

design of dowels function of a ratio

$$\beta = \frac{t}{d}$$

where t is the thickness of the wood piece and d the diameter of the dowel.

$$\beta_{\text{lim}} = 1,25 \sqrt{\frac{f_{\text{yd}}}{f_{\text{ed}}}}$$

Corresponds to the limit of the wood embedment and the steel dowel bending.

If $\beta \leq \beta_{\text{lim}}$ that means wood embedment than $R_{\text{vd},1} = 0,40 \frac{t^2}{\beta} f_{\text{ed}}$

If $\beta > \beta_{\text{lim}}$ that means dowel steel bending than

$$R_{\text{vd},1} = 0,625 \frac{d^2}{\beta_{\text{lim}}} f_{\text{yd}} \quad (\text{com } \beta = \beta_{\text{lim}})$$

where $f_{\text{yd}} = \frac{f_{\text{yk}}}{\gamma_s}$ and $\gamma_s = 1,1$



LaMEM



LaMEM

Serviceability Limit States

$$E_{co,ef} = k_{mod,1} \cdot k_{mod,2} \cdot k_{mod,3} \cdot E_{co,m}$$

- The total displacement must be less than $l/300$ of the span neither $l/150$ of the cantilever beam length.
- The displacement of dead loads can be compensate by given a camber during construction.

Constructive Recommendations

- static system must be clearly defined;
- to avoid deterioration of wood, no durable woods, must be treated with preservatives;
- the minimum areas and width of simple principal structural elements must be 50 cm² and 5 cm and 18 cm² and 2.5 cm for secondary structural elements, respectively;
- the minimum area and width of multiple principal structural elements must be 35 cm² and 2.5 cm, and 18 cm² and 1.8 cm for secondary structural elements, respectively;
- the minimum bolts diameter is 10 mm;
- the minimum number of dowels in a connection must be two;



LaMEM

LaMEM - SET - EESC - USP

Code Annexes

- drawing of timber structures;
- strength and stiffness properties of Brazilian timbers,
- test methods for strength and stiffness determination of properties of timbers;
- test methods for strength and stiffness determination of timber joints;
- recommendations of preservative treatment of wood;
- calibration of 2007 Limit States Design versus 1982 Allowable Stress Design



LaMEM

LaMEM - SET - EESC - USP



LaMEM

ACKNOWLEDGMENTS

- The author thanks the financial support of the Foundation of Support of Research of São Paulo State – FAPESP
- THANK YOU FOR YOUR ATTENTION